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(54) HAND WHEEL POSITION DETECTION SYSTEM

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	G01D 3/036	(2006.01)

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(58) Field of Classification Search

USPC701/34; 324/76.77, 141, 166 See application file for complete search history.

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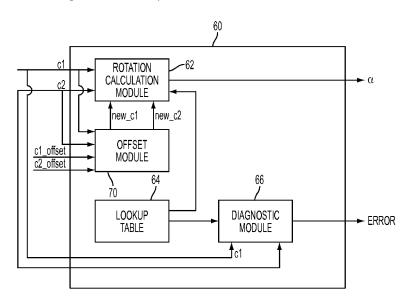
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(57) ABSTRACT

A steering system for detecting a hand wheel position is provided and includes an input shaft connected to a hand wheel, a main gear disposed around the input shaft, a puck gear meshingly engaged with the main gear, and a control module. The control module receives an angular main position of the main gear and an angular puck position of the puck gear. The control module includes a rotational calculation module for calculating the hand wheel position based on at least the angular main position and the angular puck position.

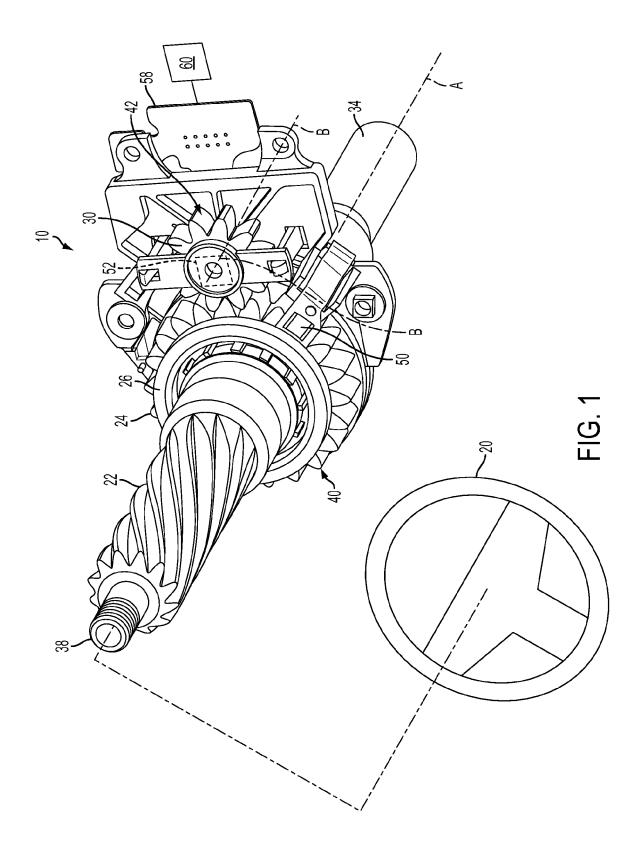
14 Claims, 6 Drawing Sheets



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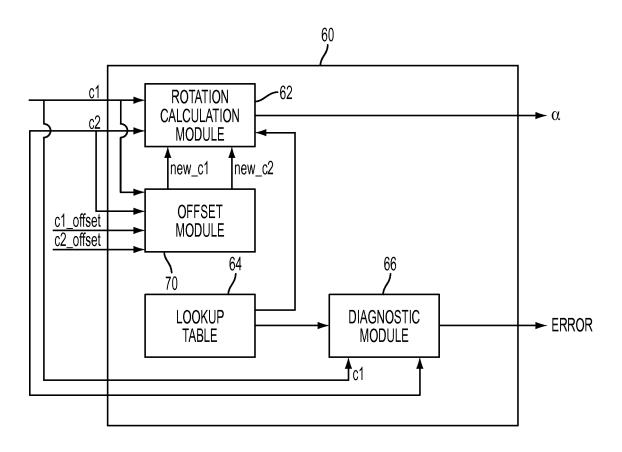


FIG. 2

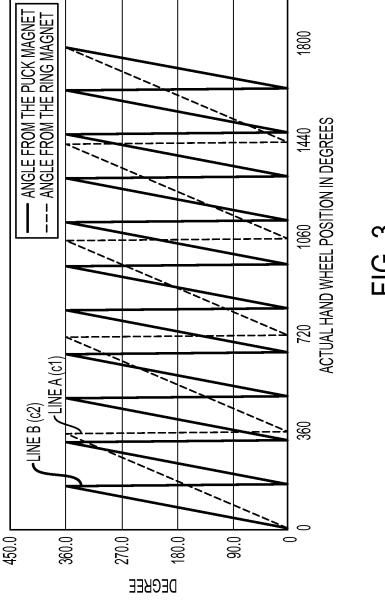
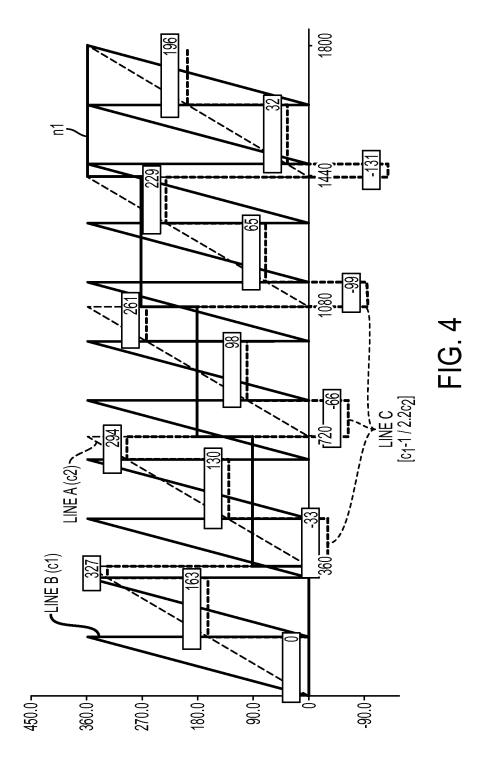
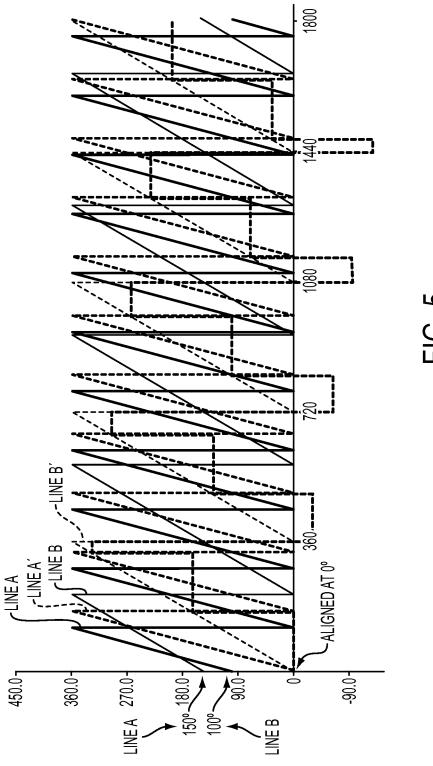
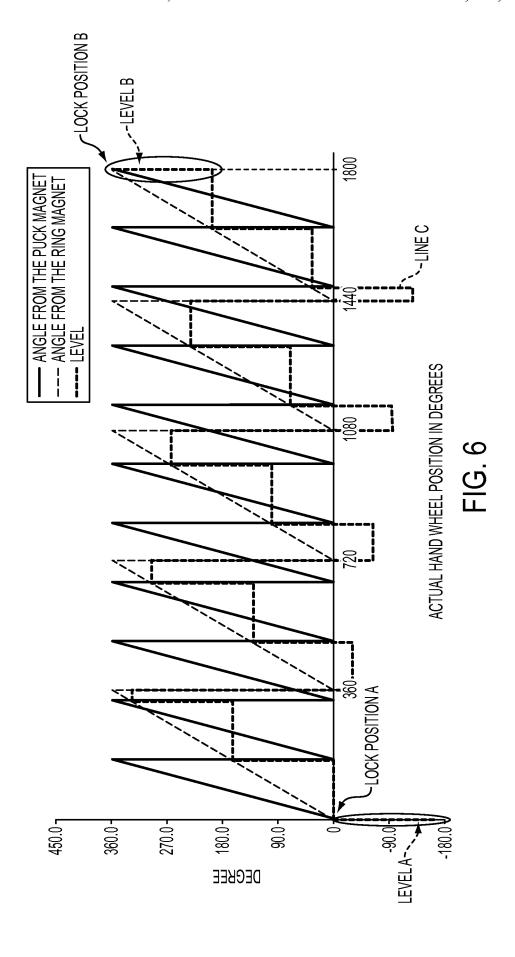


FIG. 3







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HAND WHEEL POSITION DETECTION SYSTEM

CROSS-REFERENCES TO RELATED APPLICATIONS

This patent application claims priority to U.S. Provisional Patent Application Ser. No. 61/579,770 filed Dec. 23, 2011 which is hereby incorporated herein by reference in its entirety.

BACKGROUND OF THE INVENTION

The present invention relates to a steering system, and more particularly to a steering system for detecting a hand ¹⁵ wheel position.

Some types of steering systems may require the detection of hand wheel position to provide safety features, or for certain types of algorithms. Several approaches currently exist for determining the hand wheel position. However, some of these approaches may not include the level of precision that is needed. For example, one type of hand wheel position detection system may require a five degree diagnostic limit Hand wheel position detection systems that are currently available may not be able to meet this requirement.

SUMMARY OF THE INVENTION

According to one aspect of the invention, a steering system for detecting a hand wheel position is provided. The steering 30 system includes an input shaft connected to a hand wheel, a main gear disposed around the input shaft, a puck gear meshingly engaged with the main gear, and a control module. The control module receives an angular main position of the main gear and an angular puck position of the puck gear. The 35 control module includes a rotational calculation module for calculating the hand wheel position based on at least the angular main position and the angular puck position.

According to another aspect of the invention, a steering system for detecting a hand wheel position is provided. The 40 steering system includes an input shaft connected to a hand wheel, a main gear disposed around the input shaft, a puck gear meshingly engaged with the main gear, and a control module. The control module receives an angular main position of the main gear and an angular puck position of the puck 45 gear. The control module includes a rotational calculation module for calculating the hand wheel position based on at least the angular main position and the angular puck position. The control module includes a diagnostic module for determining an error of the hand wheel position by comparing the 50 hand wheel position with a second hand wheel position.

These and other advantages and features will become more apparent from the following description taken in conjunction with the drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

The subject matter which is regarded as the invention is particularly pointed out and distinctly claimed in the claims at the conclusion of the specification. The foregoing and other 60 features, and advantages of the invention are apparent from the following detailed description taken in conjunction with the accompanying drawings in which:

FIG. 1 is an exemplary steering system for detecting a hand wheel position according to one aspect of the invention;

FIG. 2 is a dataflow diagram illustrating a control module shown in FIG. 1, according to another aspect of the invention;

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FIG. 3 is a graph illustrating an output of a first magnetic sensor and a second magnetic sensor shown in FIG. 1, according to yet another aspect of the invention;

FIG. 4 is another graph illustrating an output of a first magnetic sensor and a second magnetic sensor shown in FIG. 1, according to yet another aspect of the invention;

FIG. 5 is yet another graph illustrating an output of a first magnetic sensor and a second magnetic sensor shown in FIG. 1, according to yet another aspect of the invention; and

FIG. 6 is another graph illustrating yet another output of a first magnetic sensor and a second magnetic sensor shown in FIG. 1, according to yet another aspect of the invention.

DETAILED DESCRIPTION

Referring now to FIG. 1, where the invention will be described with reference to specific embodiments without limiting same, an exemplary embodiment of a steering system 10 is illustrated. The steering system 10 includes a hand wheel 20, an input shaft 22, a main gear 24, a ring magnet 26, a puck gear 30, and an output shaft 34. A distal end 38 of the input shaft 22 attaches to the hand wheel 20. The input shaft 22 and the output shaft 34 both extend along a longitudinal axis A-A. The steering system 10 is configured for detecting an angular position of the hand wheel 20 as the hand wheel 20 is rotated about the longitudinal axis A-A by an operator. In one embodiment, the hand wheel 20 may be rotated by an operator to manipulate a vehicle (not shown), however it is understood that the steering system 10 may be used in a variety of approaches.

The ring magnet 26 is disposed around the input shaft 22 and is located within the main gear 24. The puck gear 30 includes a puck magnet (not shown) that is molded into the puck gear 30. In the exemplary embodiment as shown in FIG. 1, the main gear 24 and the puck gear 30 are spur gears. A plurality of teeth 40 of the main gear 24 are meshingly engaged with the plurality of teeth 42 of the puck gear 30. As the input shaft 22 is rotated about the longitudinal axis A-A by the hand wheel 20, the main gear 24 rotates about the longitudinal axis A-A as well. The main gear 24 drives the puck gear 30, where the puck gear 30 rotates about a secondary axis B-B that is offset from the longitudinal axis A-A. In one embodiment, the main gear 24 and the puck gear 30 have a gear ratio of about 1:2.2.

A plurality of first magnetic field sensors 50 are provided for detecting the position of the ring magnet 26 located within the main gear 24, and plurality of second magnetic field sensors 52 are provided for detecting the position of the puck gear 30 (the second magnetic field sensor 52 is shown in phantom line). The first and second magnetic field sensors 50 and 52 may be any type of sensor for detecting the angular position of the ring magnet 36 or the puck gear 30 such as, for example, a Hall effect sensor. A control module 60 is in communication with the first magnetic field sensors 50 and the second magnetic field sensors 52 through an interface 58.

The control module 60 controls the operation of the power steering system 10. Referring now to FIG. 2, a dataflow diagram illustrates an exemplary embodiment of the control module 60 of FIG. 1 used to control the steering system 10 of FIG. 1. In various embodiments, the control module 60 may include one or more sub-modules and datastores. As used herein the terms module and sub-module refer to an application specific integrated circuit (ASIC), an electronic circuit, a processor (shared, dedicated, or group) and memory that executes one or more software or firmware programs, a combinational logic circuit, and/or other suitable components that provide the described functionality. As can be appreciated,

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the sub-modules shown in FIG. 2 can be combined and/or further partitioned to similarly determine the angular position of the hand wheel 20.

FIG. 3 is a graph illustrating the output of the first and second magnetic field sensors $\bf 50$ and $\bf 52$ as the hand wheel $\bf 20$ (shown in FIG. 1) is rotated about the longitudinal axis A-A. Specifically, FIG. 3 illustrates five revolutions of the hand wheel $\bf 20$ (which is a rotation of about 1799 degrees). FIG. 3 also shows the respective angular positions of the ring magnet $\bf 26$ (shown in FIG. 1) denoted as Line A and the puck gear $\bf 30$ 10 denoted as Line B, which range from about 0 to about 360 degrees. Referring now to both FIGS. 1-3, the control module $\bf 60$ receives as inputs the angular position from the ring magnet $\bf 26$ (shown in FIG. 1), which is denoted as $\bf c_1$, as well as the angular position from the puck gear $\bf 30$ (shown in FIG. 1), 15 which is denoted as $\bf c_2$.

FIG. 2 illustrates the control module 60 including a rotational calculation module 62, a lookup table 64, a diagnostic module 66, and an offset module 70. The rotational calculation module 62 receives as inputs the ring magnet angle c_1 and 20 the puck gear angle c_2 . A hand wheel position α is related to the ring magnet angle c_1 and the puck gear angle c_2 by equations 1-3:

$$c_1$$
= α -360 n_1 (Equation 1)
$$c_2$$
= $G\alpha$ -360 n_2 (Equation 2)
$$\alpha$$
= c_1 +360 n_1 (Equation 3)

where n_1 is the number of rotations of the input shaft 22 (having a total of 5 rotations, within the range of 0 to 1799 degrees) and n_2 is the number of rotations of the puck gear 30 (having a total of 11 rotations). Using equations 1-2 above, equation 4 may be derived as:

$$1/360[c_1-1/G c_2]=1/G n_2-n_1$$
 (Equation 4) 35

where G is the gear ratio. For a given value of n_1 and n_2 , there is a unique value for $[c_1-1/G\ c_2]$. The term $[c_1-1/G\ c_2]$ is an empirical value that is used to determine the number of rotations of the input shaft n_1 . In one approach, a gear ratio of 1:2.2 may be used (e.g., thus equation 4 would be $1/360[c_1-40.2\ c_2]=1/2.2\ n_2-n_1$). Turning now to FIG. 4, based on equation 4, the term $[c_1-1/G\ c_2]$ is plotted as a dashed line, and is referred to as Line C. Based on Line C shown in FIG. 4, the following Table 1 may be generated in a memory of the control module 60, and is saved as the lookup table 64 (shown 45 in FIG. 2):

TABLE 1

Line C Level	n_1	n_2	
0	0	0	
163	0	1	
327	0	2	
-33	1	2	
130	1	3	
294	1	4	
-66	2	4	
98	2	5	
261	2	6	
-99	3	6	
65	3	7	
229	3	8	
-131	4	8	
32	4	9	
196	4	10	

Referring now to Table 1 and FIGS. **2-4**, the rotational 65 calculation module **62** determines the value for the term $[c_1-1/G c_2]$ using Line C in FIG. **4**. It should be noted that because

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the values for Line C are substantially different from one another (i.e. each of the values for Line C have a difference of at least about thirty degrees from one another), the values are tolerable to noise. The rotational calculation module **62** then finds the value for the number of rotations of the input shaft n_1 using Table 1. The rotational calculation module **62** then calculates the value of the hand wheel position α using equation 3. For example, if the inputs into the rotational calculation module **62** are 290 for the ring magnet angle c_1 and 350 for the puck gear angle c_2 , then the term $[c_1-1/G\ c_2]$ yields 130. Referring to Table 1, if Line C (shown in FIG. **4**) has a value of 130, then n_1 is 1. Therefore, using equation 3, the hand wheel position α will be 650 degrees.

Referring to FIGS. 1 and 3-4, the respective positions of the ring magnet 26 (Line A) and the puck gear 30 (Line B) should be generally aligned at zero degrees (at the hand wheel position) to accurately calculate the hand wheel position α. However, referring now to FIG. 5, sometimes the positions of the ring magnet 26 (Line A) and the puck gear 30 (Line B) are not aligned at zero degrees. For example, FIG. 5 illustrates Line A with an offset of 150 degrees and Line B with an offset of 100 degrees. In this example, the offset module 70 includes an alignment algorithm for adjusting the values of the ring magnet angle c_1 and the puck gear angle c_2 . The alignment algorithm results in adjusted values for Line A and Line B, and are denoted as Line A' and Line B' (shown in phantom line). In one embodiment, the offset module 70 (shown in FIG. 2) calculates values for a new ring magnet angle new_c1 using the following algorithm:

where c_1 is the position of the ring magnet 26 indicated by Line A', and c_1 new is 150 degrees. A similar algorithm may be provided to calculate a new puck gear angle new_ c_2 as well.

Referring to FIGS. 1-4, during operation of the steering assembly 10, issues such as, for example, a sudden glitch in one of the signals for the ring magnet angle c₁ or the puck gear angle c_2 , noise in the signals for the ring magnet angle c_1 or the puck gear angle c₂, gear slippage between the ring magnet 50 **26** and the puck gear **30**, breakage of either the teeth **40** of the main gear 24 or the teeth 42 of the puck gear 30, gear lash, or the ring magnet 26 falling off the main gear 24 may occur. These issues may be detected by a diagnostic algorithm that is calculated by the diagnostic module 66 shown in FIG. 2. The 55 diagnostic module 66 calculates separate values for the hand wheel position α based on the ring magnet angle cl and the puck gear angle c2, respectively. Specifically, the diagnostic module 66 receives as inputs the ring magnet angle c₁ and the puck gear angle c_2 , as well as the number of rotations of the input shaft n_1 and the number of rotations of the puck gear n_2 . The diagnostic module 66 calculates the hand wheel position α using equation 3, and a second hand wheel position α' using equation 5:

$$\alpha' = (c_2 + 360 n_2)/G$$
 (Equation 5)

The diagnostic module 66 then determines the error within the hand wheel position α by comparing the hand wheel

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position α using equation 3, and a second hand wheel position α , and determining if the difference between the two values is above a threshold value. The error may be calculated by equation 6:

 $|\alpha - \alpha'| = \text{Error}$ (Equation 6)

The error in equation 6 may be set to any threshold value. In one exemplary embodiment, the error may be set to a threshold value of five degrees. Thus, if the term $|\alpha - \alpha'|$ results in more than five degrees, this indicates the error has exceeded the threshold value.

Turning now to FIG. 6, gear lashing between the main gear 24 and the puck gear 30 may occur, which may result in rollover values near a Lock Position A (located at about zero degrees) and a Lock Position B (located at about 1799 degrees). Thus, Line C may include additional values, where a Level A value and a Level B value is included. In the exemplary embodiment as shown, the Level A value is about -163 degrees and the Level B value is about 359 degrees.

While the invention has been described in detail in connection with only a limited number of embodiments, it should be readily understood that the invention is not limited to such disclosed embodiments. Rather, the invention can be modified to incorporate any number of variations, alterations, substitutions or equivalent arrangements not heretofore described, but which are commensurate with the spirit and scope of the invention. Additionally, while various embodiments of the invention have been described, it is to be understood that aspects of the invention may include only some of the described embodiments. Accordingly, the invention is not to be seen as limited by the foregoing description.

Having thus described the invention, it is claimed:

1. A steering system for detecting a hand wheel position, 35 comprising:

an input shaft connected to a hand wheel;

a main gear disposed around the input shaft;

- a puck gear meshingly engaged with the main gear; and
- a control module, implemented in a hardware processor, 40 for:
 - receiving an angular main position of the main gear and an angular puck position of the puck gear;
 - setting an empirical value equal to c_1 -1/G c_2 , wherein c_1 is the angular main position, c_2 is the angular puck 45 position, an G is the gear ratio;
 - finding a number of rotations of the input a number of rotations of the puck gear using the empirical value; calculating a first hand wheel position based on the number of rotations of the input shaft;
 - calculating a second hand wheel position based on the number of rotations of the puck gear; and
 - determining that the first hand wheel position is incorrect if a difference between the first hand wheel position and the second wheel position is above a threshold value.
- 2. The steering system as recited in claim 1, wherein the control module uses equations: $c_1=\alpha-360n_1$, $c_2=G$ $\alpha-360n_2$, and $\alpha=c_1+360n_1$, wherein α is the hand wheel position, n_1 is a number of rotations of the input shaft, and n_2 is a number of rotations of the puck gear.
- 3. The steering system as recited in claim 2, empirical values computed by the term $[c_1$ 1/G $c_2]$ differ from one another by at least thirty degrees depending on the angular main position c_1 , the angular puck position c_2 , the hand wheel 65 position α , the number of rotations of the input shaft n_1 , and the number of rotations of the puck gear n_2 .

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- **4**. The steering system as recited in claim **1**, wherein a position of the main gear and a position of the puck gear are aligned generally at zero degrees.
- **5**. The steering system as recited in claim **1**, wherein a position of the main gear and a position of the puck gear are offset from zero degrees.
- **6**. The steering system as recited in claim **5**, wherein the control module is further configured for executing an alignment algorithm for adjusting the position of the main gear and the position of the puck gear.
- 7. The steering system as recited in claim 1, wherein the control module is further for finding a number of rotations of the puck gear using the empirical value.
- **8**. The steering system as recited in claim 1, wherein the control module calculates the second hand wheel position using an equation: $\alpha'=(c_2+360n_2)/G$, wherein α' is the second hand wheel position, and n_2 is a number of rotations of the puck gear.
- A steering system for detecting a hand wheel position,comprising:

an input shaft connected to a hand wheel;

a main gear disposed around the input shaft;

a puck gear meshingly engaged with the main gear; and a control module, implemented in a hardware processor,

receiving an angular main position of the main gear and an angular puck position of the puck gear;

- setting an empirical value equal to c_1 1/G c_2 wherein c_1 is the angular main position, c_2 is the angular puck position, α is the hand wheel position, an G is the gear ratio:
- finding a number of rotations of the input shaft from a lookup table saved in a memory of the control module using the empirical value; and
- calculating the hand wheel position based on the number of rotations of the input shaft,
- wherein the hand wheel position is related to the angular main position and the angular puck position by: $c_1 = \alpha 360n \ 1$, $c_2 = G \ \alpha 360n_2$, and $\alpha = c_1 + 360n_1$, wherein α is the hand wheel position, n_1 is the number of rotations of the input shaft, and n_2 is a number of rotations of the puck gear.
- 10. The steering system as recited in claim 9, wherein empirical values computed by the result of c_1 1/G c_2 differ from one another by at least thirty degrees depending on the angular main position c_1 , the angular puck position c_2 , the hand wheel position α , the number of rotations of the input shaft n_1 , and the number of rotations of the puck gear n_2 .
- 11. The steering system as recited in claim 9, wherein a position of the main gear and a position of the puck gear are aligned generally at zero degrees.
- 12. The steering system as recited in claim 9, wherein a position of the main gear and a position of the puck gear are offset from zero degrees.
- 13. The steering system as recited in claim 12, wherein the control module is further configured for executing an alignment algorithm for adjusting the position of the main gear and the position of the puck gear.
- 14. The steering system as recited in claim 9, wherein the control module is further for finding a number of rotations of the puck gear from the lookup table using the empirical value, and wherein the second hand wheel position is calculated by using an equation:

 $\alpha' = (c_2 + 360n_2)/G$

wherein α' is the second hand wheel position.

* * * * *